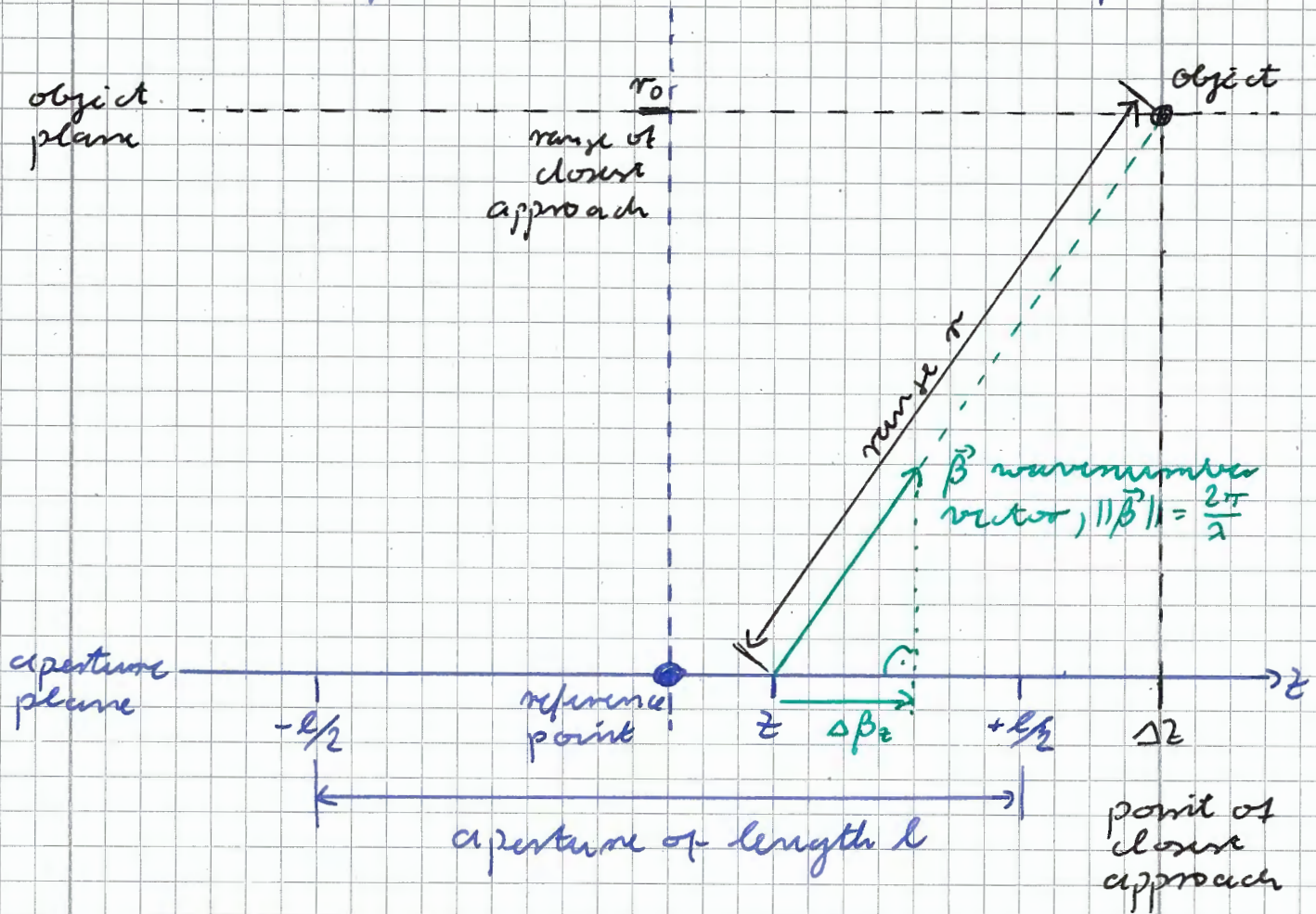


Radar Imaging

Furmanio

- for simplicity one dimensional aperture



- large aperture
 - \Rightarrow object in the near-field
 - \Rightarrow wavenumber $\Delta\beta_z$ depends on z
- small aperture
 - \Rightarrow object in the far field
 - \Rightarrow wavenumber $\Delta\beta_z$ independent of z
- real aperture: fixed transmitter
 - \Rightarrow one way channel
- synthetic aperture: transmitter and receiver at z
 - \Rightarrow two way channel, additional factor 2 in the phase shifts

Range

- near-field \Rightarrow exact

$$r(z) = \sqrt{(z - \Delta z)^2 + r_0^2} \Rightarrow \text{hyperbola}$$

- parabolic approximation
(Fresnel approximation)

$$r(z) \approx r(z_0) + \underbrace{\frac{\partial r}{\partial z} \Big|_{z_0}}_{\frac{z_0 - \Delta z}{r(z_0)}} (z - z_0) + \frac{1}{2} \underbrace{\frac{\partial^2 r}{\partial z^2} \Big|_{z_0}}_{\frac{r_0^2}{r^3(z_0)}} (z - z_0)^2$$

$$\text{e.g. } z_0 = \Delta z, \quad r(\Delta z) = r_0$$

$$\Rightarrow r(z) \approx r_0 + \frac{(z - \Delta z)^2}{2r_0} = r_0 + \frac{z^2 - 2z\Delta z + \Delta z^2}{2r_0}$$

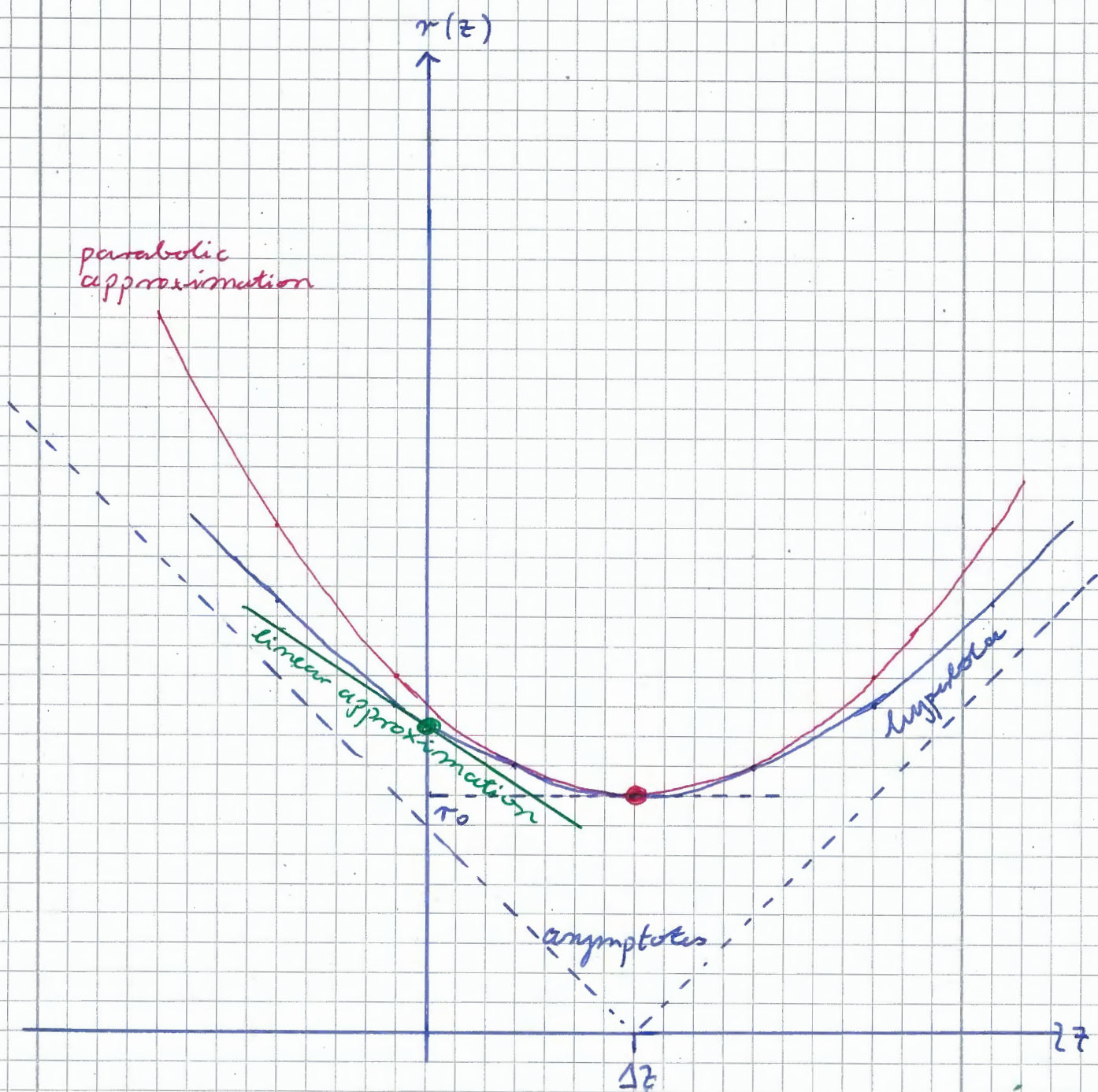
- far-field \Rightarrow linear approximation
(Fraunhofer approximation)

$$r(z) \approx r(z_0) + \underbrace{\frac{\partial r}{\partial z} \Big|_{z_0}}_{\frac{z_0 - \Delta z}{r(z_0)}} (z - z_0)$$

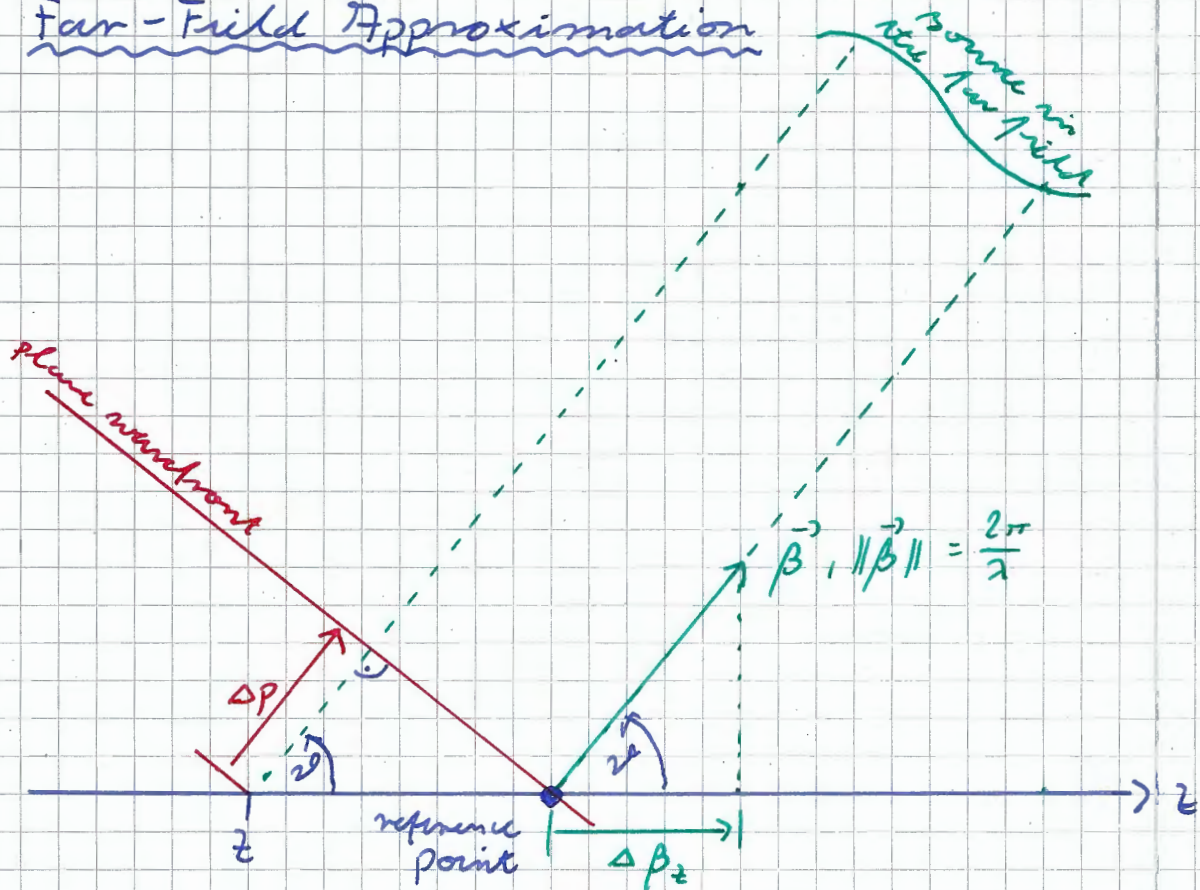
$$\text{e.g. } z_0 = 0, \quad r(0) = \sqrt{\Delta z^2 + r_0^2}$$

$$\Rightarrow r(z) \approx r(0) - \underbrace{\frac{\Delta z}{r(0)}}_{\cos \vartheta} z$$

$$\cos \vartheta = \frac{\partial \beta_z}{\|\vec{\beta}\|} = \frac{\lambda}{2\pi} \Delta \beta_z$$



Far-Field Approximation



- one way channel
- path length difference

$$\Delta P = -z \cos \theta \quad (\text{in the figure } z \text{ is negative})$$

- phase shift

$$\varphi = -2\pi \frac{\Delta P}{\lambda} = 2\pi \frac{z \cos \theta}{\lambda}$$

$$\text{using } \Delta \beta_z = \frac{2\pi}{\lambda} \cos \theta$$

$$\varphi = \Delta \beta_z z \quad \text{linear in } z!$$

Received Signal, Far-Field Approximation

- one way channel
- received signal at reference point \underline{E}_{RP}
- narrowband approximation

$$\underline{e}(z) = \underline{E}_{RP} e^{-j \frac{2\pi}{\lambda} (r(z) - r(0))}$$

- far-field approximation of $r(z)$

$$\underline{e}(z) \approx \underline{E}_{RP} e^{-j \frac{2\pi}{\lambda} (r(0) - \frac{1}{2\pi} \Delta\beta_z z - r(0))}$$

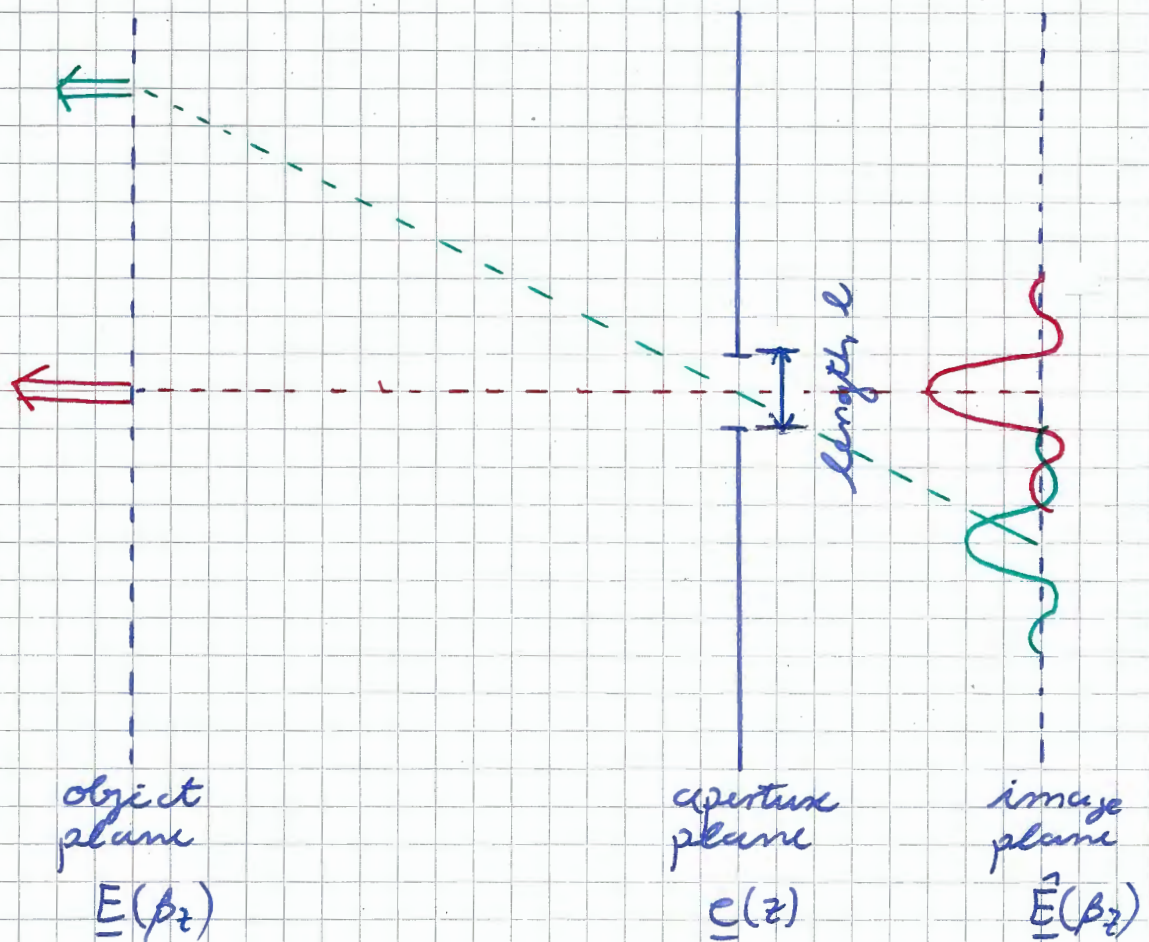
$$= \underline{E}_{RP} e^{j \Delta\beta_z z}$$

$$\begin{array}{c} z \circ \\ \beta_z \circ \end{array}$$

$$\underline{E}(\beta_z) = \int \underline{e}(z) e^{-j \beta_z z} dz \approx 2\pi \underline{E}_{RP} \delta(\beta_z - \Delta\beta_z)$$

\Rightarrow image $\underline{E}(\beta_z)$ is the Fourier transform of the signal $\underline{e}(z)$ in the aperture plane

Example: Pinhole Camera



finite aperture

- rectangular window $\text{rect}(\frac{z}{l})$ in spatial domain
- convolution with sinc -function in wavenumber domain!

$$\begin{aligned}\hat{E}(\beta_z) &= \mathcal{F}\{e(z) \text{rect}(\frac{z}{l})\} = \hat{\mathcal{F}}\{e(z)\} * \mathcal{F}\{\text{rect}(\frac{z}{l})\} \\ &= \underline{E}(\beta_z) * \text{sinc}(\frac{\beta_z}{2})\end{aligned}$$

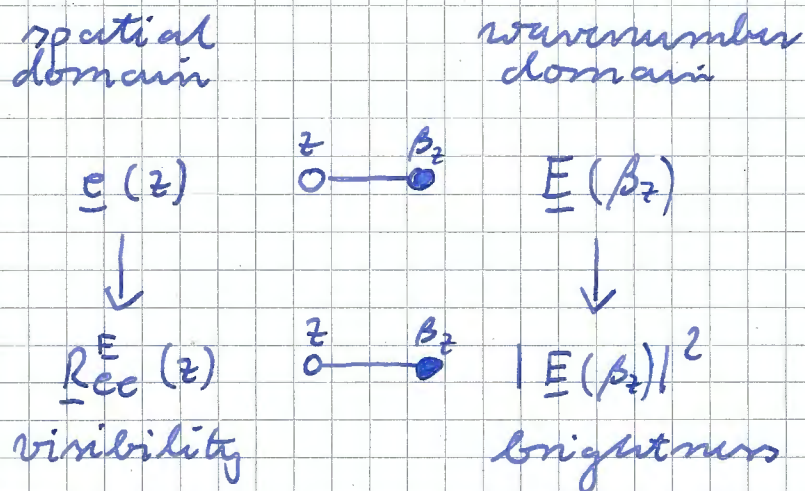
\Rightarrow large aperture \Leftrightarrow high resolution
(less diffraction)

as long as the far-field approximation holds

Example: Real Aperture Radar (RAR)

- In contrast to the pinhole camera, the wavefield is measured in the aperture plane using antennas.
- Often, only the brightness $|\underline{E}(\beta_z)|^2$ is of interest.
- The visibility is the autocorrelation function of the received signal $\underline{c}(z)$ in the aperture plane:

$$\begin{aligned}\mathcal{F}^{-1}\{|\underline{E}(\beta_z)|^2\} &= \mathcal{F}^{-1}\{\underline{E}^*(\beta_z) \underline{E}(\beta_z)\} \\ &= \underline{c}^*(-z) * \underline{c}(z) = \underline{c}_{cc}^E(z)\end{aligned}$$



- Typically, real apertures are relatively small
 \Rightarrow far-field approximation holds but low resolution

Resolution of Real Aperture Radar (RAR)

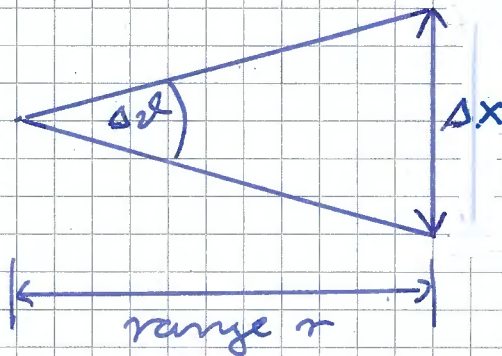
- direction of arrival (DOA) resolution

$$\Delta \theta \approx \frac{\lambda}{2l} \text{ wavenumber resolution}$$

\uparrow
 $\theta \approx \frac{\pi}{2}$

$$\approx \frac{\lambda}{l}$$

- cross-range resolution



$$\Delta x \approx r \Delta \theta \approx \frac{\lambda r}{l}$$

\uparrow
small $\Delta \theta$

\Rightarrow large real aperture l required

\Rightarrow low resolution for large range r

\Rightarrow not suitable for remote sensing

Received Signal, Parabolic Approximation

- one way channel
- parabolic approximation of $r(z)$ and $r(0)$

$$\underline{e}(z) = \underline{e}_{RP} e^{-j \frac{2\pi}{\lambda} (r(z) - r(0))}$$

$$\approx \underline{e}_{RP} e^{-j \frac{2\pi}{\lambda} \left(r_0 + \frac{z^2 - 2z\Delta z + \Delta z^2}{2r_0} - r_0 - \frac{\Delta z^2}{2r_0} \right)}$$

$$= \underline{e}_{RP} e^{-j \frac{2\pi}{\lambda} \frac{z^2 - 2z\Delta z}{2r_0}}$$

- focusing (for a certain range of closest approach r_0 , independent of Δz)

$$\underline{e}(z) \underbrace{e^{j \frac{2\pi}{\lambda} \frac{z^2}{2r_0}}}_{\approx 1 \text{ for } r_0 \rightarrow \infty} \approx \underline{e}_{RP} e^{j \frac{2\pi}{\lambda} \frac{z\Delta z}{r_0}} = \underline{e}_{RP} e^{j \Delta \beta_z z}$$

$$\approx 1 \text{ for } r_0 \rightarrow \infty$$

(focusing ineffective
in the far-field)

$$\text{using } \Delta \beta_z = \frac{2\pi}{\lambda} \underbrace{\frac{\Delta z}{r_0}}$$

$\propto \cos \theta$ in the far field

\Rightarrow After focusing, the signal is the same as in the case of the far-field approximation.

The image $\underline{E}(\beta_z)$ can now be computed using the Fourier transform.

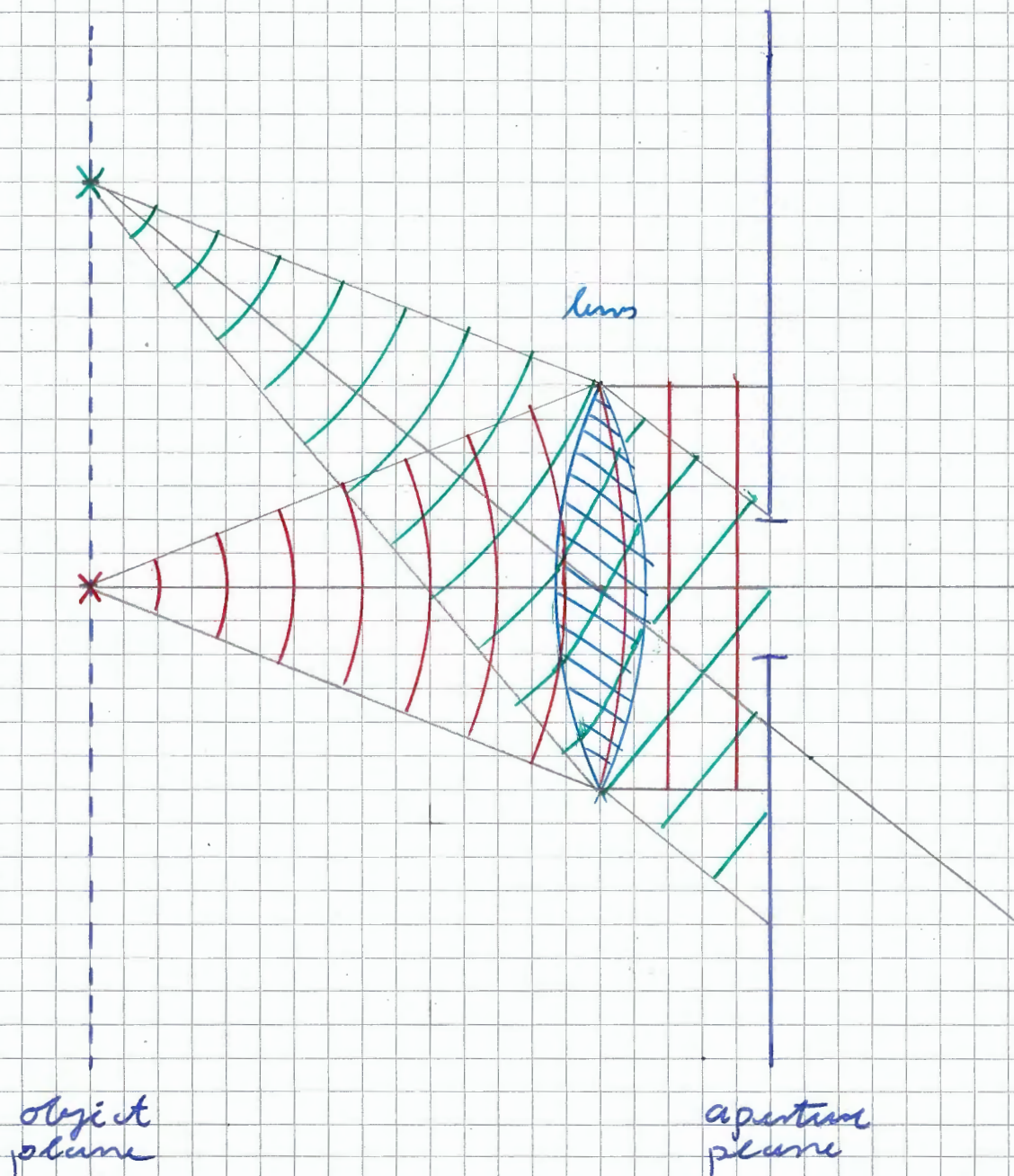
Lens

lens introduces a

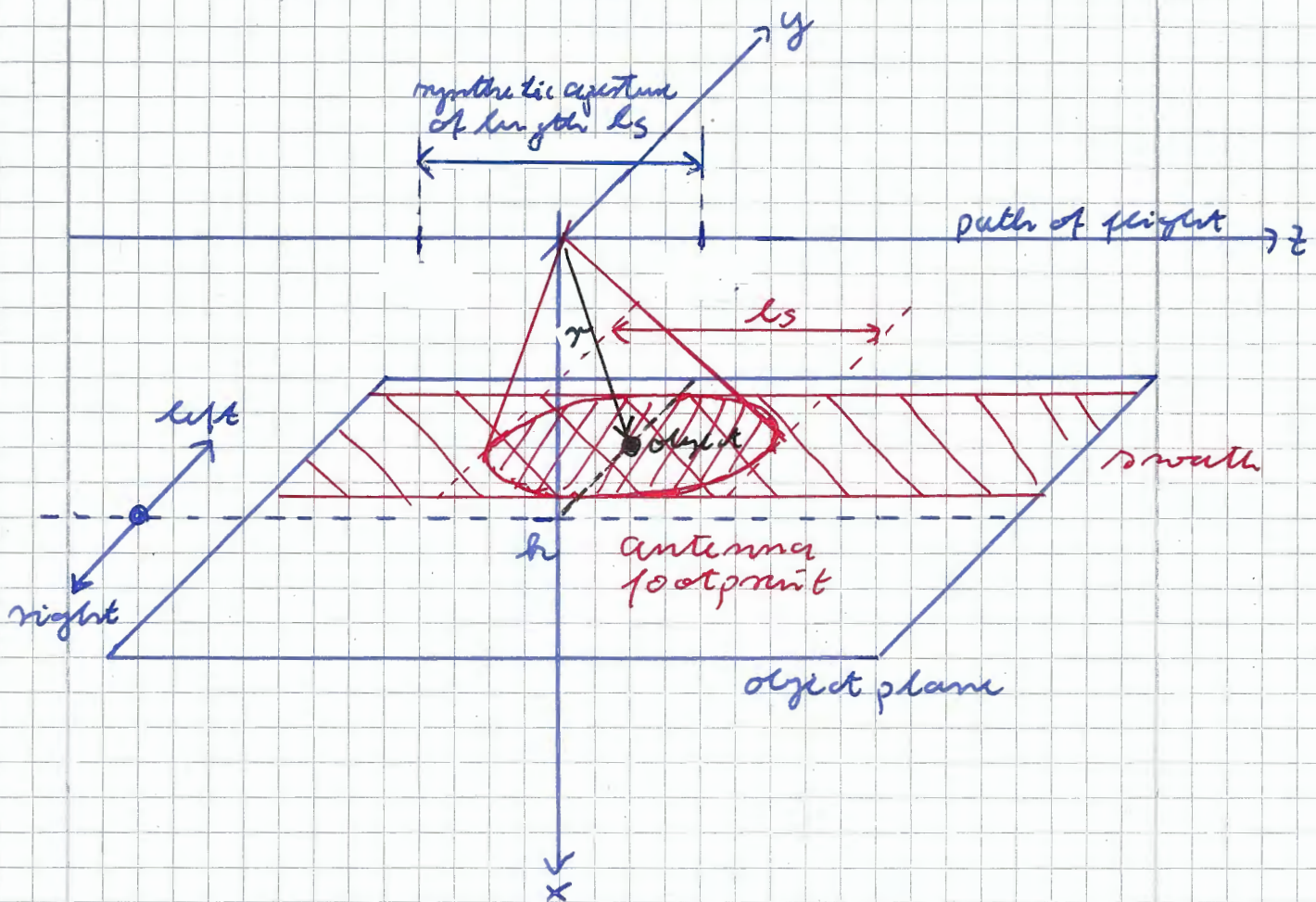
$$\text{delay} \sim -z^2$$

\Rightarrow can be implemented using a lens

\Rightarrow the spherical wave in the near-field is transformed into a plane wave (as in the far-field)



Example: Synthetic Aperture Radar (SAR)



- path of flight at height h above the object plane
- take measurements of the wavefield on the path of flight
⇒ synthetic aperture
- resolve left-right-ambiguity using a directive antenna
⇒ side looking synthetic aperture radar (SAR)
- length l_s of the synthetic aperture equals the length of the antenna footprint

Cone of Constant Wavenumber

The intersection of the cone of constant wavenumber $\Delta\beta_z$ and the object plane is a hyperbola of constant wavenumber $\Delta\beta_z$.

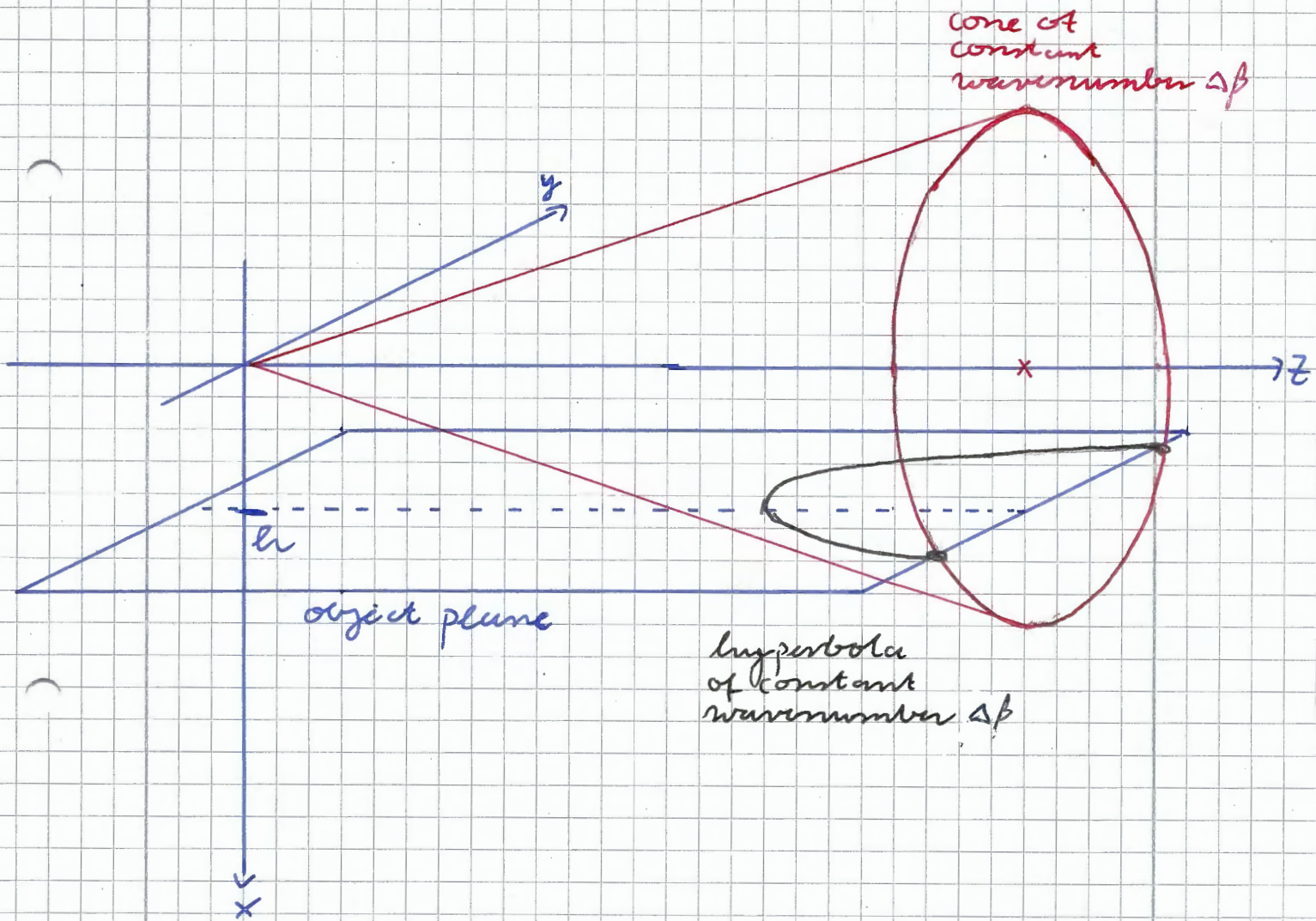
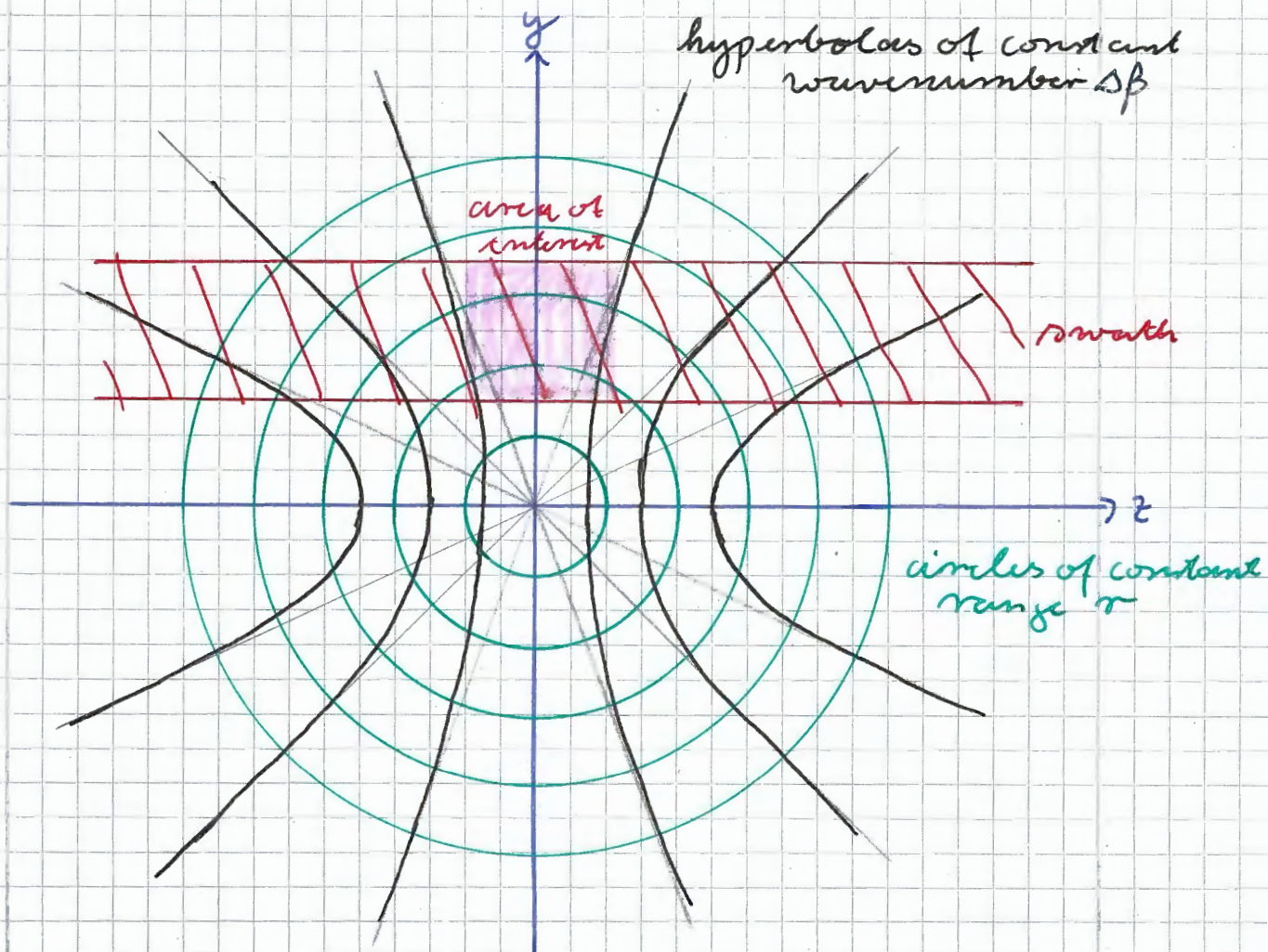


Image Formation in Synthetic Aperture Radar (SAR)

- measure
 - range r (delay Δt) and
 - wavenumber $\Delta\beta_z$ (direction of arrival θ , DOA)on the one-dimensional synthetic aperture
- compute a two-dimensional image exploiting
 - circles of constant range r and
 - hyperbolas of constant wavenumber $\Delta\beta$ in the object plane

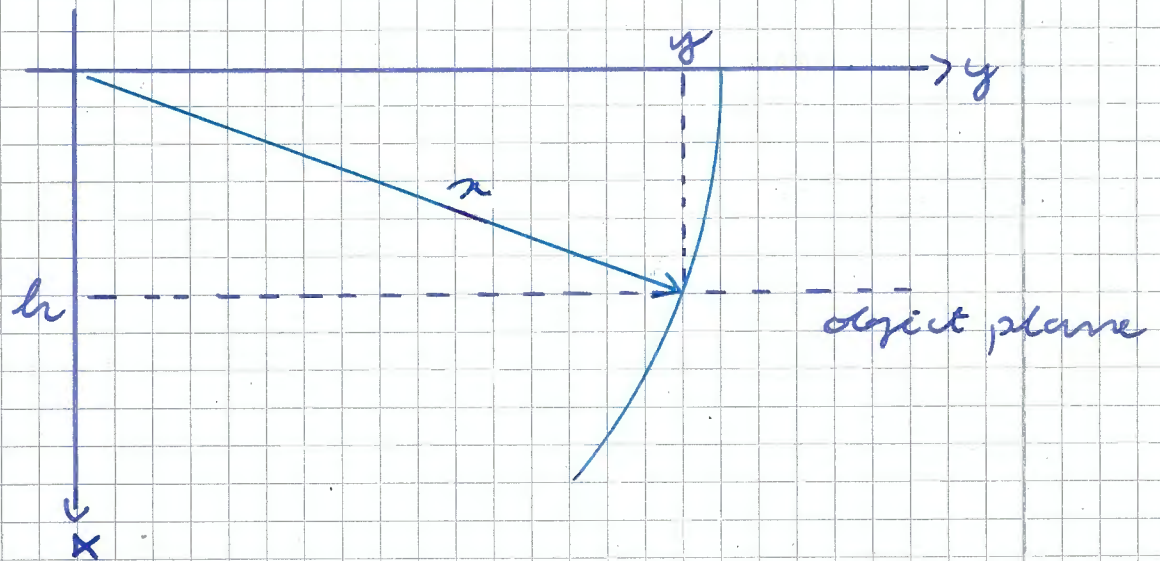


Cross-Track Resolution of Synthetic

Aperture Radar (SAR)

- cross-track $\hat{=}$ y
- area of interest: $\Delta z \approx 0$, $h \ll y$

$$\Rightarrow y \approx r$$



- cross-track resolution

$$\approx \text{range resolution}$$

$$\approx \frac{c_0}{2} \text{ time resolution}$$

$$\approx \frac{\pi c_0}{\text{bandwidth}}$$

(factor $\frac{1}{2}$ due to two way channel)

\Rightarrow independent of range r

\Rightarrow suitable for remote sensing

Along-Track Resolution of Synthetic

Aperture Radar (SAR)

- length l_R of real aperture
- length of the antenna footprint is equal to the length of the synthetic aperture

$$l_s = \frac{\lambda r}{l_R} \quad \text{the cross-range resolution of real aperture radar (RAR)}$$

- along-track $\hat{=}$ z
- area of interest: $\Delta z \approx 0$, $h \ll y$
 \Rightarrow along-track \approx cross-range
- along-track resolution

\propto cross-range resolution

$$\approx \frac{\lambda r}{2l_s} = \frac{1}{2} l_R$$

(factor $\frac{1}{2}$ due to two way channel)

\Rightarrow smaller real apertures yield higher resolution in synthetic aperture radar (SAR)

\Rightarrow independent of range r

\Rightarrow suitable for remote sensing