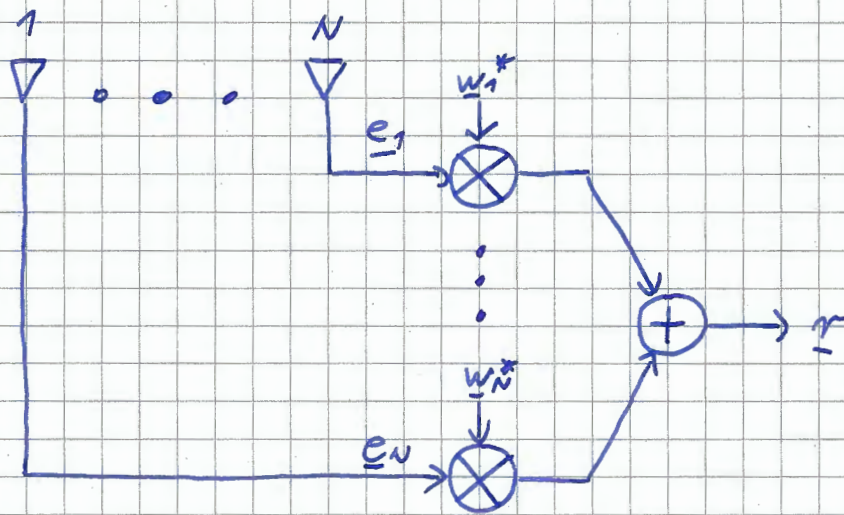


Beamforming Network

Beamforming Network



- weights: \underline{w}^*

- weight vector:

$$\underline{w}^* = \begin{pmatrix} w_1^* \\ \vdots \\ w_N^* \end{pmatrix}$$

- idea:

adjust the weights such that the phase shifts (steering factors) for a certain direction of arrival are compensated

\Rightarrow signals from this direction of arrival will superimpose constructively

- antenna array together with the beamforming network acts like a directional antenna

Received Signal

- received vector:

$$\underline{e} = \begin{pmatrix} \underline{e}_1 \\ \vdots \\ \underline{e}_N \end{pmatrix}$$

- signal at the output of the beamforming network:

$$\underline{r} = \sum_n \underline{w}_n^* \underline{e}_n = \underline{w}^{*T} \cdot \underline{e}$$

- (instantaneous) power at the output of the beamforming network:

$$P_r = |\underline{r}|^2 = |\underline{w}^{*T} \cdot \underline{e}|^2 \leq \|\underline{w}\|^2 \|\underline{e}\|^2$$

↑
Cauchy inequality

- passive beamforming network:

$$P_r \leq \|\underline{w}\|^2 \|\underline{e}\|^2 \leq \|\underline{e}\|^2 = P$$

$$\Rightarrow \|\underline{w}\|^2 \leq 1$$

- in the following:

$$\|\underline{w}\|^2 = 1 \quad \text{"lossless"}$$

Antenna gain

- consider a single source:
 - single direction of arrival φ
 - single array manifold vector $\underline{a}(\varphi)$
 - single source signal \mathcal{P}_{RP}
- received vector:

$$\underline{r} = \underline{a}(\varphi) \cdot \mathcal{P}_{RP}$$

$$\Rightarrow \underline{r} = \underbrace{\underline{w}^{*T} \cdot \underline{a}(\varphi)}_{\substack{F(\varphi) \\ \text{array factor}}} \cdot \mathcal{P}_{RP}$$

- antenna gain:

$$\begin{aligned} g(\varphi) &= |F(\varphi)|^2 \\ &= |\underline{w}^{*T} \cdot \underline{a}(\varphi)|^2 \\ &= \underline{w}^{*T} \cdot \underbrace{\underline{a}(\varphi) \cdot \underline{a}^{*T}(\varphi)}_{\text{positive semidefinite matrix}} \cdot \underline{w} \geq 0 \end{aligned}$$

- antenna pattern:

antenna gain normalized to its maximum value

$$C(\varphi) = \frac{g(\varphi)}{g(\varphi_{\max})} = \frac{\underline{w}^{*T} \cdot g(\varphi) \cdot \underline{a}^{*T}(\varphi) \cdot \underline{w}}{\underline{w}^{*T} \cdot \underline{a}(\varphi_{\max}) \cdot \underline{a}^{*T}(\varphi_{\max}) \cdot \underline{w}}$$

plotted as a function of the direction of arrival φ

Example: Uniform Linear Array

- array factor:

$$\underline{F} = \underline{w}^* \cdot \underline{a} = \sum_n \underline{w}_n^* \underline{a}_n$$

- Using

$$\underline{a}_n = \underline{\varepsilon}^{-\frac{N-1}{2}} \underline{\varepsilon}^n$$

one obtains:

$$\underline{F}(\underline{\varepsilon}) = \underline{\varepsilon}^{-\frac{N-1}{2}} \underbrace{\sum_n \underline{w}_n^* \underline{\varepsilon}^n}$$

corresponds to a z-transform

\Rightarrow Design of beamforming networks is a filter design problem (spatial filter).

Aliasing

- $\underline{\varepsilon} = e^{j d \beta_x}$

and consequently also

- the array factor \bar{I} ,
- the antenna gain g and
- the antenna pattern G'

are periodic functions of β_x .

- Periodic repetitions of the main lobe of the antenna pattern G' are called grating lobes.

- period:

$$-\pi \leq d \beta_x \leq +\pi$$

- visible region:

$$-\frac{2\pi}{\lambda} \leq \beta_x \leq +\frac{2\pi}{\lambda}$$

=> no visible periodicity if

$$d \frac{2\pi}{\lambda} \leq +\pi$$

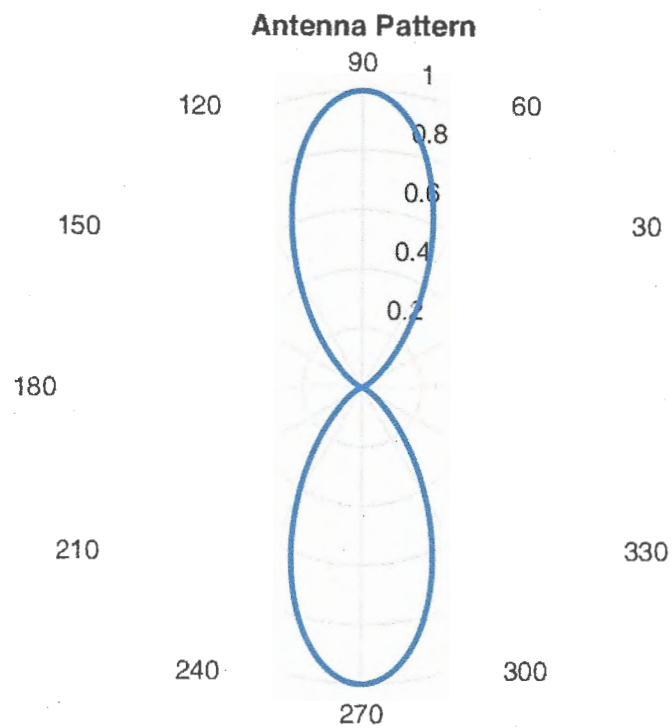
$$d \leq \frac{\lambda}{2}$$

ULA

$$N=4$$

$$d=0.25\lambda$$

$$\underline{W}^T = \frac{1}{2} \begin{pmatrix} 1 \\ 1 \\ 1 \\ 1 \end{pmatrix}$$



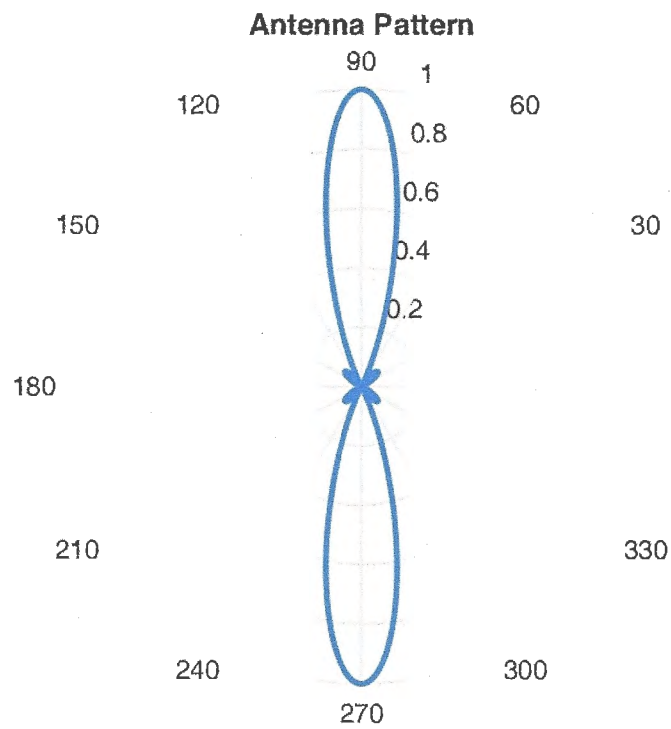
↑ 4
—

ULB

$N=4$

$d=0.5\lambda$

$$\underline{w^*} = \frac{1}{2} \begin{pmatrix} 1 \\ 1 \\ 1 \\ 1 \end{pmatrix}$$

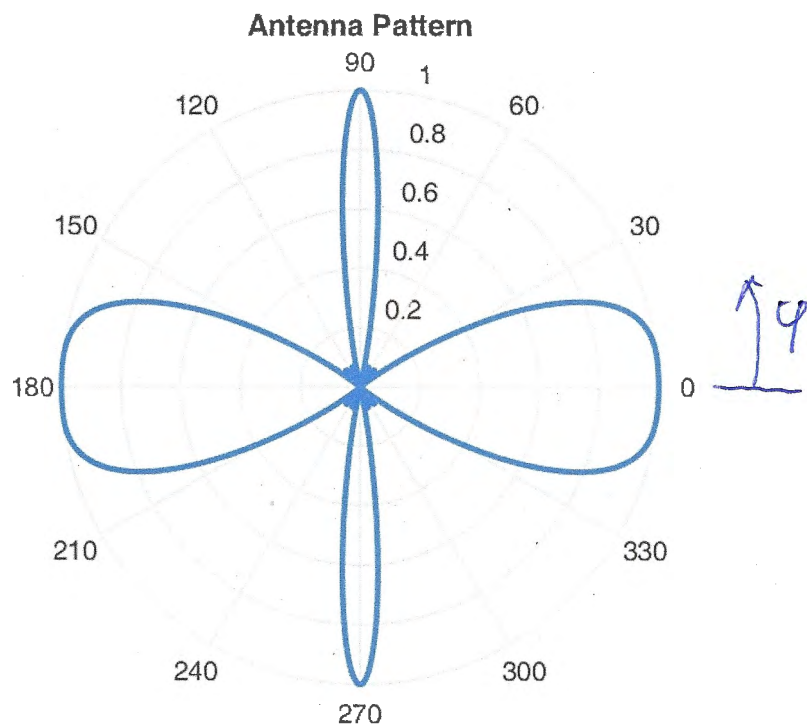


ULA

$N=4$

$d = \lambda$

$$\underline{w^*} = \frac{1}{2} \begin{pmatrix} 1 \\ 1 \\ 1 \\ 1 \end{pmatrix}$$



Power at the Output of the Beamforming Network

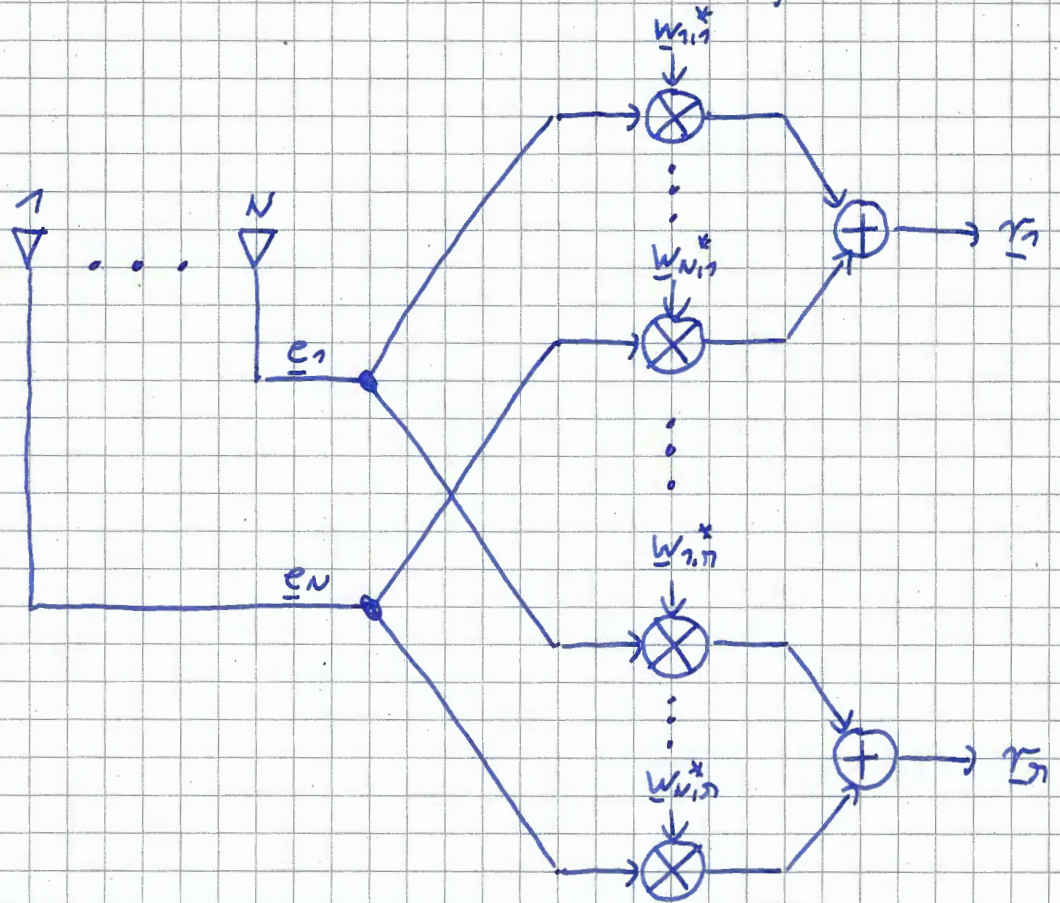
several sources and noise

$$\begin{aligned}\Rightarrow P_r &= E\{|r|^2\} \\ &= E\{\underline{w}^{*T} \cdot \underline{e} \cdot \underline{e}^{*T} \cdot \underline{w}\} \\ &= \underline{w}^{*T} \cdot E\{\underline{e} \cdot \underline{e}^{*T}\} \cdot \underline{w} \\ &= \underline{w}^{*T} \cdot \underline{R}_{ee} \cdot \underline{w}\end{aligned}$$

All the relevant information
about the received signals is
contained in the correlation matrix \underline{R}_{ee} .

Beamspace

- use N beamforming networks in parallel:



- received vector in beamspace:

$$\underbrace{\begin{pmatrix} \underline{r}_1 \\ \vdots \\ \underline{r}_n \end{pmatrix}}_{\underline{r}} = \underbrace{\begin{pmatrix} \underline{w}_{1,1}^* & \dots & \underline{w}_{N,1}^* \\ \vdots & & \vdots \\ \underline{w}_{1,n}^* & \dots & \underline{w}_{N,n}^* \end{pmatrix}}_{\underline{W}^{*T}} \cdot \underbrace{\begin{pmatrix} \underline{e}_1 \\ \vdots \\ \underline{e}_N \end{pmatrix}}_{\underline{e}}$$

weight matrix

- invertible weight matrix:

\Rightarrow one-to-one mapping, no loss of information

- Fourier matrix as a weight matrix

\Rightarrow Butler matrix, low cost implementation similar to fast Fourier transform